

IMPROVED STRUCTURAL SANDWICH PLATE MEMBERS

The present invention relates to structural sandwich plate members which comprise
5 two outer plates and a core of plastics or polymer material bonded to the outer plates with
sufficient strength to substantially contribute to the structural strength of the member.

Structural sandwich plate members are described in US 5,778,813 and US 6,050,208,
which documents are hereby incorporated by reference, and comprise outer metal, e.g. steel,
plates bonded together with an intermediate elastomer core, e.g. of unfoamed polyurethane.
10 These sandwich plate systems may be used in many forms of construction to replace stiffened
steel plates, formed steel plates, reinforced concrete or composite steel-concrete structures
and greatly simplify the resultant structures, improving strength and structural performance
(e.g. stiffness, damping characteristics) while saving weight. Further developments of these
structural sandwich plate members are described in WO 01/32414, also incorporated hereby
15 by reference. As described therein, foam forms may be incorporated in the core layer to
reduce weight and transverse metal shear plates may be added to improve stiffness.

According to the teachings of WO 01/32414 the foam forms can be either hollow or
solid. Hollow forms generate a greater weight reduction and are therefore advantageous. The
forms described in that document are not confined to being made of light weight foam
20 material and can also be made of other materials such as wood or steel boxes.

International Patent Application WO 02/078948 is a further development of the
concept of including hollow forms and describes forms that are easy to manufacture and
assemble, in particular hollow elongate forms made from snap-together pieces are described.

The basic forms of structural sandwich plate members described in US 5,778,813 and
25 US 6,050,208 have excellent fire resistance properties, even without structural fire protection.
Unlike stiffened steel plates with external structural fire protection which may be damaged or
blown free of the plate during an explosion or blast load event, the elastomer core of the
structural sandwich plate member, which provides fire resistance, is internal and remains intact
and functional.

30 Structural sandwich plate members according to US 5,778,813 and US 6,050,208 also
provide greater protection against ballistics threats than conventional steel plating. For
example, tests have demonstrated that a 3-30-3 structural sandwich plate member (3mm mild

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steel-30mm polyurethane-3mm mild steel) offers 70% greater protection against 7.62mm calibre bullets than a conventional stiffened steel plate of comparable weight. However, further improvement is still necessary to meet standards such as the US National Institute of Justice standard NIJ 0108.01.

5 Existing forms of armour intended to resist projectiles often comprise a combination of hard, e.g. ceramic, plates and layers of high-tensile strength fabric, e.g. Kevlar(TM) or Spectra(TM), however these arrangements are expensive to manufacture, heavy and vulnerable to damage to the plates in ordinary use of the item.

10 It is an aim of the present invention to provide structural sandwich plate members that have improved resistance to explosions and projectiles.

According to the present invention, there is provided: a structural sandwich plate member comprising: first and second outer plates; a core of plastics or polymer material bonded to said outer plates with sufficient strength to transfer shear forces therebetween; and
15 at least one interlayer within the core, said interlayer being generally parallel to the outer plates and having a higher tensile strength than the core material.

The provision of an interlayer or interliner within the core provides a substantial improvement in the blast and/or projectile resistance of the plate member, much greater than would be expected merely from the addition of the extra material. Exactly what form the
20 interlayer should take depends on the threat to be protected against.

For blast protection, an additional metal, e.g. steel or aluminium, layer of similar dimensions to the outer layers is preferred. This ensures that even if one of the outer layers is penetrated by shrapnel or completely stripped away by the force of the explosion, a sandwich structure with substantial strength and fire insulation properties remains. A solid metal plate
25 also provides additional protection against projectiles.

For increased ballistic resistance and protection only, a more lightweight layer such as metal (e.g. steel) mesh or a high tensile strength fabric, such as Kevlar(TM) or Spectra(TM) may be employed. Such a layer obstructs or restrains any projectiles that penetrate the outer metal layer and captures any fragments of the outer metal layer or the core layer generated by
30 the impact of the projectile. Ceramic sheets may also be used to provide ballistics and/or blast protection.

Preferably the interlayer is corrugated or dimpled. This increases the chances that the projectile engages more of the interlayer and at more favourable impact angles.

Multiple interlayers may be provided to further improve ballistics or blast resistance. If multiple corrugated or dimpled interlayers are provided, the corrugations and/or dimples in
5 the different layers may have different orientations and/or offsets.

The materials, dimensions and general properties of the outer plates of the structural sandwich plate member of the invention may be chosen as desired for the particular use to which the structural sandwich plate member is to be put and in general may be as described in US-5,778,813 and US-6,050,208. Steel or stainless steel is commonly used in thicknesses of
10 0.5 to 20mm and aluminium may be used where light weight is desirable. Similarly, the plastics or polymer core may be any suitable material, for example an elastomer such as polyurethane, as described in US-5,778,813 and US-6,050,208.

Further, the invention provides a method of manufacturing a structural sandwich plate member comprising the steps of: providing first and second outer plates in a spaced-apart
15 relationship with at least one interlayer located therebetween and spaced from each of said outer metal plates; injecting uncured plastics or polymer material to fill the space defined between said outer plates and either side of said interlayer; and allowing said plastics or polymer material to cure to bond said outer plates together with sufficient strength to transfer shear forces therebetween; wherein said interlayer has a higher tensile strength than the cured
20 plastics or polymer material.

Where the interlayer is completely or significantly impervious to the uncured plastics or polymer material, the injection of the core can be carried out from both sides of the plate, either simultaneously or in two stages.

The interlayer may be coated or impregnated with plastics or polymer material prior to
25 insertion into the cavity between the outer metal plates to give additional rigidity so that the interlayer maintains its shape and position during the injection process, e.g. where the interlayer is a high tensile strength fabric, and/or to improve bonding to the core material. If not the same as the core material, the plastics or polymer material with which the interlayer is coated or impregnated should be compatible with the core material.

30 The present invention will be described below with reference to exemplary embodiments and the accompanying schematic drawings, in which:

Figure 1 is a cross-sectional view of a structural sandwich plate member according to a first embodiment of the present invention;

Figure 2 is a cross-sectional view of a structural sandwich plate member according to a second embodiment of the present invention;

5 Figure 3 is a cross-sectional view of a structural sandwich plate member according to a third embodiment of the present invention;

Figure 4 is a cross-sectional view of a structural sandwich plate member according to a fourth embodiment of the present invention;

10 Figure 5 is a cross-sectional view of a structural sandwich plate member according to a fifth embodiment of the present invention; and

Figure 6 is a cross-sectional view of a structural sandwich plate member according to a sixth embodiment of the present invention;

In the various drawings, like parts are indicated by like reference numerals.

15 The structural sandwich plate member shown in Figure 1 comprises upper and lower outer plates (faceplates) 11, 12 which may be of steel or aluminium and have a thickness, for example, in the range of from 0.5 to 20mm. A thickness of greater than or equal to 3mm is advantageous in many applications. Edge plates are welded between the face plates 11, 12 around their outer peripheries to form a closed cavity. In the cavity between the face plates
20 11, 12 is a core 13 of plastics or polymer material, preferably a compact thermosetting material such as polyurethane elastomer. This core may have a thickness in the range of from 15 to 200mm; in the present application 50mm is suitable. The core 13 is bonded to the face plates 11, 12 with sufficient strength and has sufficient mechanical properties to transfer shear forces expected in use between the two face plates. The bond strength between the core 13 and face
25 plates 11, 12 should be greater than 3MPa, preferably 6MPa, and the modulus of elasticity of the core material should be greater than 200MPa, preferably greater than 250MPa, especially if expected to be exposed to high temperatures in use. For low load applications, such as floor panels, where the typical use and occupancy loads are of the order of 1.4kPa to 7.2kPa, the bond strength may be lower, *e.g.* approximately 0.5MPa. By virtue of the core layer, the
30 structural sandwich plate member has a strength and load bearing capacity of a stiffened steel plate having a substantially greater plate thickness and significant additional stiffening. The plate, of course, need not be flat but may take any form required for its intended use.

To improve the resistance of the material to ballistic projectiles, an interlayer 14 of high tensile strength fabric is provided in the core 13. As illustrated, the interlayer 14 is positioned in the middle of core 13 but this may be varied, provided a reasonable amount of core material remains either side of the interlayer. The interlayer should have a high tensile strength, for example similar to that of steel, and other properties, such as a high modulus of elasticity and high visco-elasticity, to assist in resisting projectiles, as is known. Several layers of fabric or netting may be used to provide the desired strength. The interlayer may extend throughout the sandwich plate or may be localised to those areas requiring protection. The thickness of the interlayer need not be uniform, similarly additional material may be provided where most protection is desired.

Suitable materials include fibres made of molecular chains produced from poly-paraphenylene terephthalamide (aramids), preferably as sold by E. I. du Pont de Nemours and Company under the brand name Kevlar(TM). Suitable grades include Kevlar 29, Kevlar KM2, Kevlar 129 and Kevlar 49. Also suitable are fibres made from ultra-high molecular weight polyethylene, preferably as sold by Honeywell Performance Fibres under the brand name Spectra(TM). Other suitable materials include para-aramid fibres, preferably as sold by Teijin Limited under the brand names Technora (TM) and Twaron(TM).

Where light weight is desired, the core may include lightweight forms as described in WO 01/32414. Preferably, the forms are made of fire-resistant materials as described in Copending British patent application 0306195.9 filed 18 March 2003. Particular advantages can be achieved with forms made of non-tessellating shapes as described in British patent application no 0326608.7 (Agent's ref N90171) entitled "IMPROVED STRUCTURAL SANDWICH PLATE MEMBERS WITH FORMS" filed 14 November 2003. As described therein, the forms may be made of hard materials to increase ballistics resistance and fragment capture. These documents are incorporated herein in their entirety by reference.

To manufacture the structural sandwich plate member 10, the edge plates are welded around the periphery of lower faceplate 11 and then the interlayer 14 and spacers to hold it in place are placed in the resulting open cavity. At this stage, any precast sections of the core may be put in place as well as any shear plates or other fittings that may be desired. Then, the upper faceplate 12 is welded to the edge plates to form a closed cavity and the plastics or polymer material injected to form core 13. The injected material is then allowed to cure and the injection ports used in the injection step ground off and sealed along with the vent holes.

These steps may be performed in situ, or off-site in factory conditions and the finished panel transported to the installation site.

To improve the handling of the fabric forming the interlayer, it may be coated or impregnated with a plastics or polymer material so as to be more rigid prior to insertion in the cavity. The impregnation or coating material may be the same as used to form the core material but if not should be compatible therewith, e.g. bond well to the core material. The bond strength between the core and the fabric interlayer 14 should not be less than that between the core and the faceplates 11 & 12. In some cases the fabric may have to be chemically treated to ensure sufficient bond to the core 13.

If the fabric is dense, especially if several layers are provided, so that it is not easily penetrated by the uncured core material, injection of the core material can be performed from both sides of the plate, either simultaneously or sequentially.

A second embodiment of the present invention is shown in Figure 2. The structural sandwich plate member 20 according to the second embodiment of the invention is similar to the first embodiment but different in the nature of the interlayer, as described below.

In the second embodiment, the interlayer 15 comprises a metal, e.g. steel, stainless steel or aluminium, plate, forming a multiple layered structural sandwich plate member. The metal plate is generally formed of the same material as the outer plates but need not necessarily be so. The thickness of the metal plate 15 depends on the amount of ballistic or blast protection desired and the required residual structural strength. In many cases, a metal plate acting as interlayer will have the same thickness as one of the outer metal layers but may differ from this by $\pm 50\%$.

The second embodiment is manufactured in the same general way as the first embodiment save that impregnation or coating of the metal plate is not generally necessary. Instead, the metal plate is cleaned and/or pretreated in the same way as the faceplates to give equivalent bond strength to the core 13. The metal plate 15 can simply be tack welded or glued to supports to keep it in place during injection.

Figure 3 illustrates a third embodiment of the present invention which differs from the second embodiment in that the interlayer 16 is perforated. The perforations provide weight saving, enhance the bond to the core by mechanical interlock and allow the uncured core material to flow freely throughout the cavity. Suitable perforated plates may have regular patterns of holes of sizes in the range of from 3 to 20mm and density, expressed as the ratio

of the total area of holes to the total plan area of the plate, in the range of from 0.25 to 0.5. Such plates are widely available. Variations on the hole pattern, size and density may be effected to enhance ballistic and blast resistance. The perforated plates may be made of hard ceramic materials as well as metals.

5 As an alternative to a perforated plate, a metal mesh may be used. This is illustrated in Figure 4 which shows a fourth embodiment of the invention. The mesh not only provides the same advantages as the third embodiment but also has varying orientation of the interlayer with respect to the faceplates which provides greater ballistic resistance, in particular for bullets fired at between 45 and 90° to the plating. Expanded steel mesh such as steel mesh no
10 1292 manufactured by the Expanded Metal Company Limited of Hartlepool, England is suitable for use in the invention. This has a mesh size (centre-centre) of 30.48mm x 12.70mm, a strand width of 4.75mm and thickness of 2.5mm and a total open area of 25%. The mesh size, strand width and thickness and total open area may be selected as a function of the ballistic threat to be resisted and the level of resistance required.

15 Figure 5 shows a further variant of the first embodiment, in which the interlayer 18 has a zig-zag corrugated form. For most projectiles, this arrangement maximises the amount of material of the interlayer that the projectile contacts and ensures that projectiles that impact the outer layer perpendicularly will be incident on the inter layer at an acute angle, increasing the effective penetration strength of the interlayer. If the interlayer is of high tensile strength
20 fabric, the zig-zag shape can be effected by impregnating the fabric with a thermosetting material in a suitably shaped mould. In the case of metal or metal mesh layers, the zig-zag shape may be applied by roll-forming or pressing.

As shown in Figure 6, as an alternative to a zig-zag shape, the interlayer may be provided with wavy corrugations. This has a similar effect and can be achieved in similar
25 ways. Figure 6 also illustrates the use of multiple, in this case two, interlayers 19a, 19b, which may be offset from each other (as shown) or oriented perpendicular to each other. Dimpled interlayers, or sheets corrugated in two directions, may also be used.

It will be appreciated that the above description is not intended to be limiting and that
30 other modifications and variations fall within the scope of the present invention, which is defined by the appended claims.